

Power System Analysis
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Lecture - 6
Transmission Line Capacitance (Contd.)

Welcome to lesson 6 on Power System Analysis. In this lesson, we are going to discuss Transmission Line Capacitance which we were discussing in lessons 5. We are continuing with it.

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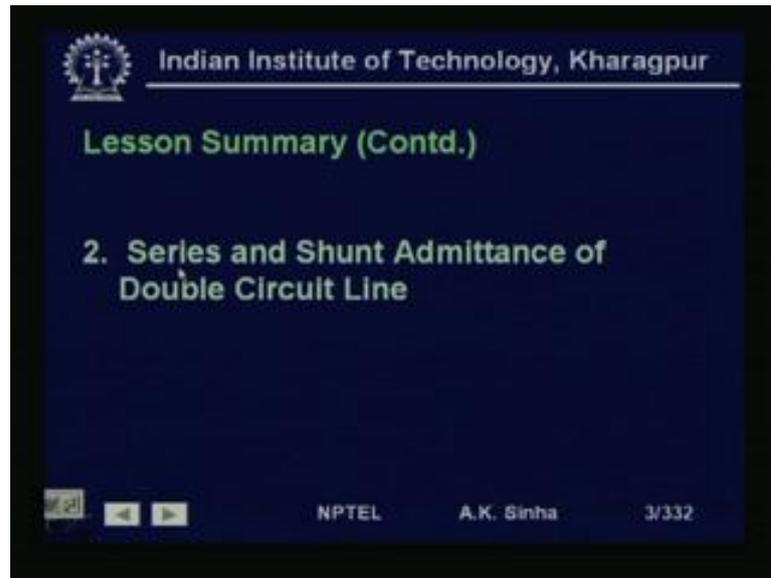


The slide is a dark blue presentation slide with white and yellow text. At the top left is the IIT Kharagpur logo. The text on the slide reads: 'Indian Institute of Technology, Kharagpur' in white, followed by 'Lesson 6' in yellow, 'TRANSMISSION LINE CAPACITANCE (Contd.)' in yellow, and 'Lesson Summary' in white. Below this is a numbered list: '1. Effect of earth on Transmission Line Capacitance for:' followed by 'a) Single phase line' and 'b) Three phase line with earth return'. At the bottom, there are small icons for navigation and the text 'NPTEL A.K. Sinha 2/32'.

Here, what we will do is, we will consider the effect of earth on transmission line capacitance. Actually when we have this transmission lines, the phase conductors are in above the ground in over a transmission system. And the distance between the phase conductors and ground are of the same magnitude. And therefore, the earth which acts as a equipotential surface. Thus effect the electric field lines and thereby the capacitors.

So, we need to consider the effect of earth. And calculating the capacitance for transmission lines. So, in these lessons we will discuss, how the earth or the ground affects the capacitance of a single phase transmission line, and how it affects the three phase transmission line.

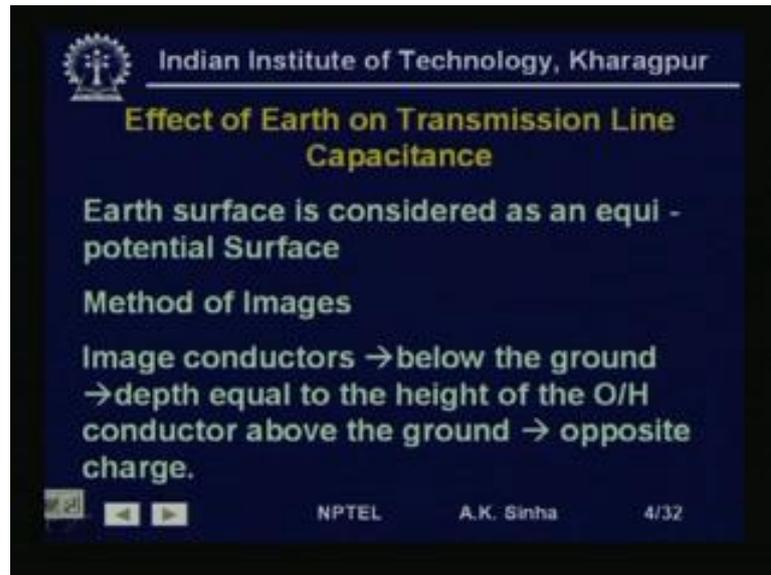
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Then, we will talk about a double circuit line. And we will talk about how we calculate the series, and shunt impedance of the double circuit line. In fact, when we have a double circuit line the two circuits are somewhat close to each other. That is the three phase conductors of one circuit and the three phase conductors of the other circuit, are most of the time placed on the same tower. And therefore, they are in quite close proximity.

And because of which the both the magnetic field lines, as well as electric field line do get effected by the currents flowing in the other circuit. And the voltages present in the phase conductors in the other circuit. Therefore, for a double circuit line, we have the mutual effects. Because of the two circuits and that needs to be considered. And we will see how we take care of this, in this lesson. Well, we will first start with the effect of earth on transmission line capacitance.

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Effect of Earth on Transmission Line Capacitance

Earth surface is considered as an equipotential surface

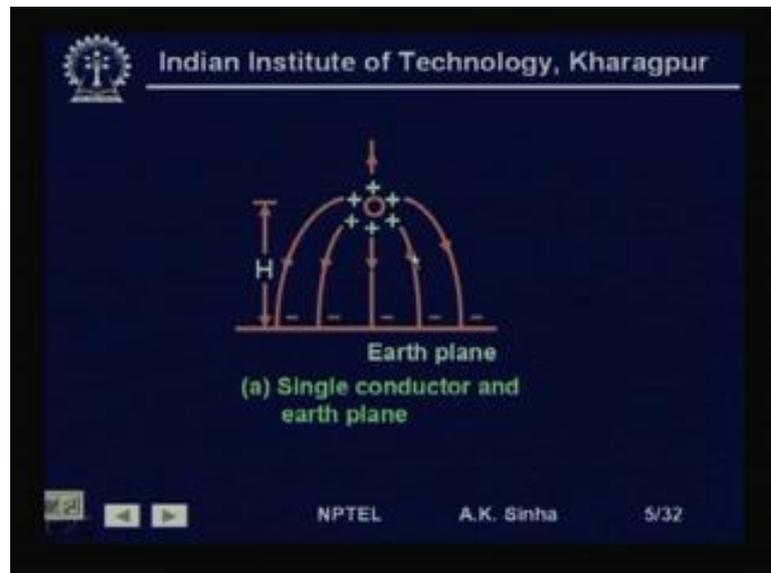
Method of Images

Image conductors → below the ground
→ depth equal to the height of the O/H conductor above the ground → opposite charge.

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Now, as I said earlier, we consider the earth surface as an equipotential surface. Now, the earth surface may not be a plane. It may be undulating, it may not be horizontal, it may incline. But, for our purpose of calculation we will always consider that to be a horizontal plane surface.

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Earth plane

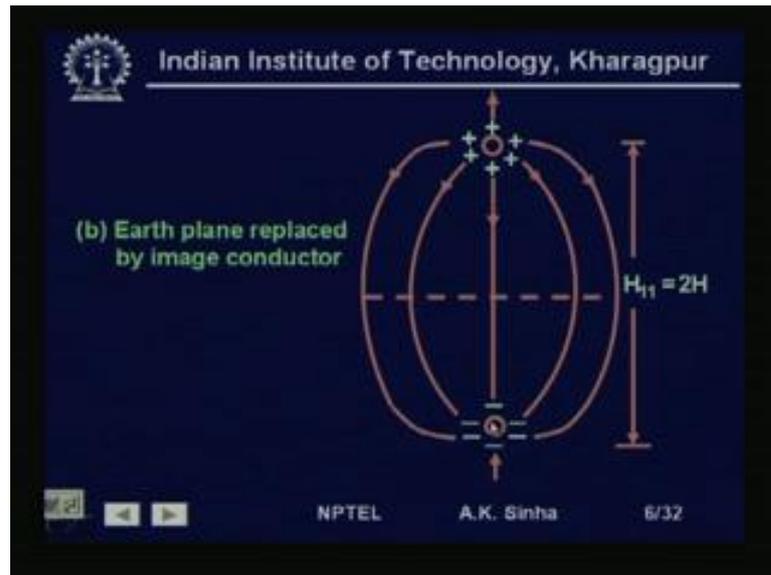
(a) Single conductor and earth plane

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Now, if we see that there is a conductor as shown here. The phase conductor, which is charged with positive charge q per meter length, then the lines of electrical lines or field line should be radiating from this in radial direction. But, because the earth is acting as

an equipotential surface. So, these field lines will bend and go to the negative potential on the earth. So, the effect of earth is to change the configuration of the electric field lines. And thereby, this will affect the capacitance of the conductor system. Now, how do we take care of this effect. Well, what we do is, we use what we call as method of images.

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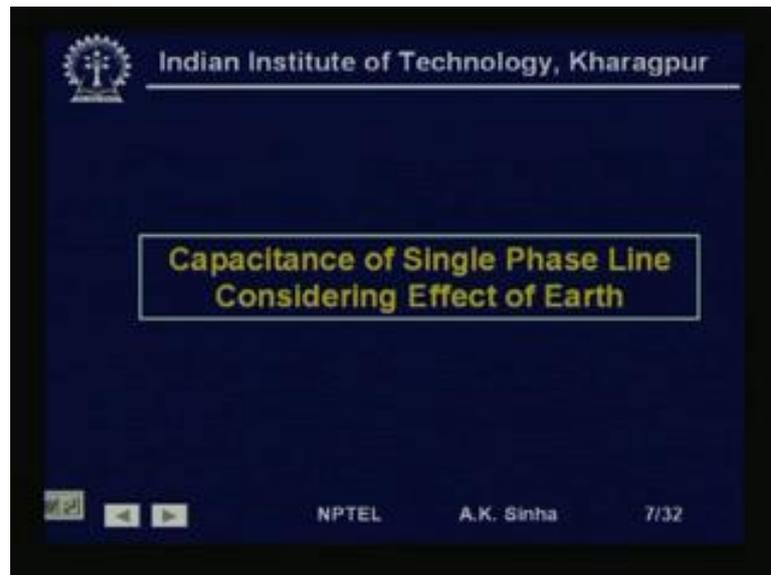
Now, in this what we do is, we consider a conductor directly below the overhead conductor in the ground at a distance; which is equal to the height of the conductor above the ground. That is we are considering an image of this conductor below the ground. So, this is a mirror image of this conductor. And the charge on the image conductor is opposite of that of the overhead conductor. Now, if you see, if you have such a system, then the field lines will look like as shown here.

Now, these field lines if you see are very much similar to if we had as just this conductor, and the ground and consideration. Therefore, what we find as that, that if we take another conductor with an opposite charge. And place it below the ground, just below the ground of this conductor at a distance, which is equal to the height of the conductor above the ground.

Then, the field lines created are exactly same as that, if this conductor as above that earth surface. That is the effect of earth can be taken care of by this kind of a situation. So, the method of images basically consist of considering image conductors below the ground at

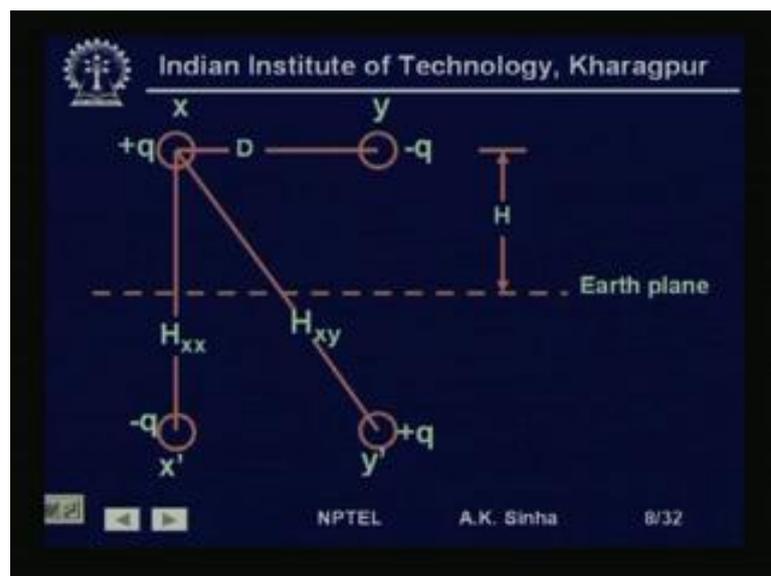
a depth; equal to the height of the overhead conductor above the ground. And the charge on this image conductor is of the opposite polarity. So, if we do this then we have a system which is consistent of the same effect as that of the earth. Now, we will try to use this for calculating the capacitance of a single phase line.

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So, capacitance of a single phase line considering the effect of earth.

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Now, here we have a single phase line with two conductors x and y. Placed at a distance D, the conductors have a radius of r_x and r_y . The charge on conductor x is q coulombs

per meter and charge on conductor is minus q coulombs per meter, because conductor y in a single phase system will be acting as a return conductor. That is current flowing in x will be returning through conductor y. Now, this system of conductors single phase 2 conductors are above the ground at a height of H meters.

So, if we have to now take the effect of ground or earth. Then, what we have to do is, we have to consider image conductor x dash, which is placed directly below the conductor x. At a distance equal to H below the ground, that is the distance between conductor x. And it is image H x x will be equal to 2 H. And the charge on this image conductor x dash will be minus q coulombs per meter.

Similarly, we will consider the image conductor for conductor y, as y dash which will be placed directly below the conductor y at a distance of 2 H. That is at a distance H below the ground directly under conductor y. And the charge on this conductor y dash will be equal to plus q per coulomb per meter. So, now with this system we would like to find out the voltage between the two conductors x and y.

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$$V_{xy} = \frac{q}{2\pi\epsilon} \left[\ln \frac{D_{yx}}{D_{xx}} - \ln \frac{D_{yy}}{D_{xy}} - \ln \frac{H_{yx}}{H_{xx}} + \ln \frac{H_{yy}}{H_{xy}} \right]$$

$$= \frac{q}{2\pi\epsilon} \left[\ln \frac{D_{yx} D_{xy}}{D_{xx} D_{yy}} - \ln \frac{H_{yx} H_{xy}}{H_{xx} H_{yy}} \right]$$

$$= \frac{q}{\pi\epsilon} \left[\ln \frac{D}{r} - \ln \frac{H_{xy}}{H_{xx}} \right]$$

We can write this voltage from the earlier lesson, that we have had. We can write this voltage V_{xy} is equal to q by twice pi epsilon into $\log n D_{yx}$. That is the distance of the conductor b to conductor a divide by D_{xx} . That is the distance of conductor a to conductor a, that is conductor x to conductor x. So, in similar way we will write for the charge on conductor y, considering the charge on conductor y.

We will have the relationship q by twice π epsilon minus q by twice π epsilon D_{yy} . That is the distance of conductor y to conductor y itself divided by distance of conductor x from y . Now, due to the image conductor x' , we will have the effect on the voltage given by q by minus q by twice π epsilon $\log_n \frac{H_{yx}}{H_{xx}}$. That is distance of image conductor x' to conductor y . And H_{xx} that is divided H_{xx} , that is the distance between x and the image conductor x' .

For the charge on the conductor y' , we will have the term q by twice π epsilon $\log_n \frac{H_{yy}}{H_{xy}}$. Now, if we consider all these terms together. And arrange them, then we will get this as equal to q by twice π epsilon $\log_n \frac{D_{yx}}{D_{xy}} \times \frac{D_{xx}}{D_{yy}}$. That is this minus $\log_n \frac{D_{yy}}{D_{xy}}$ by D_{xx} can be written as plus $\log_n \frac{D_{xx}}{D_{yy}}$. And then we can add these two together that will get me $\log_n \frac{D_{yx}}{D_{xy}} \times \frac{D_{xx}}{D_{yy}}$.

Similarly, considering these two conductors, this if we make it as negative then this becomes $\frac{H_{xy}}{H_{yy}}$. So, this will be minus $\log_n \frac{H_{xy}}{H_{yy}}$. Therefore, if we add these two, then we will get minus $\log_n \frac{H_{yx}}{H_{xy}} \times \frac{H_{xx}}{H_{yy}}$. Now, considering the symmetry of the figure, that we have H_{xx} will be equal to H_{yy} and H_{xy} will be equal to H_{yx} . Also D_{xx} is equal to r_x and D_{yy} is equal to r_y and if both the conductor have the same radius, then we will have that equal to r .

Therefore, this can become as $\frac{D_{yx}}{D_{xy}}$ and $\frac{D_{xx}}{D_{yy}}$ are basically equal to D . So, this becomes q by twice π epsilon $\log_n \frac{D^2}{r^2}$, which can be written as this square can be taken out. So, this will have 2 here and 2 will cancel with this 2. So, it will become q by π epsilon $\log_n \frac{D}{r}$. In the similar $\frac{H_{xy}}{H_{yy}}$ is equal to $\frac{H_{yx}}{H_{xx}}$. So, this becomes equal to $\frac{H_{xy}^2}{H_{xx}^2}$ and $\frac{H_{xy}}{H_{xx}}$ is equal to $\frac{H_{yx}}{H_{yy}}$ which is equal to $\frac{H_{xy}^2}{H_{xx}^2}$, therefore this square term can be taken here. So, 2 will cancel with this 2 here, so we get q by π epsilon minus $\log_n \frac{H_{xy}}{H_{xx}}$. So, this way we have calculated the voltage between the 2 phase conductors x and y for a single phase line.

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The slide is from the Indian Institute of Technology, Kharagpur. It contains the following text and formulas:

The line-to-line capacitance is

$$C_{xy} = \frac{q}{V_{xy}} = \frac{\pi\epsilon}{\ln \frac{D}{r} - \ln \frac{H_{xy}}{H_{xx}}} \quad \text{F/m}$$
$$C_n = 2C_{xy} = \frac{2\pi\epsilon}{\ln \frac{D}{r} - \ln \frac{H_{xy}}{H_{xx}}} \quad \text{F/m}$$

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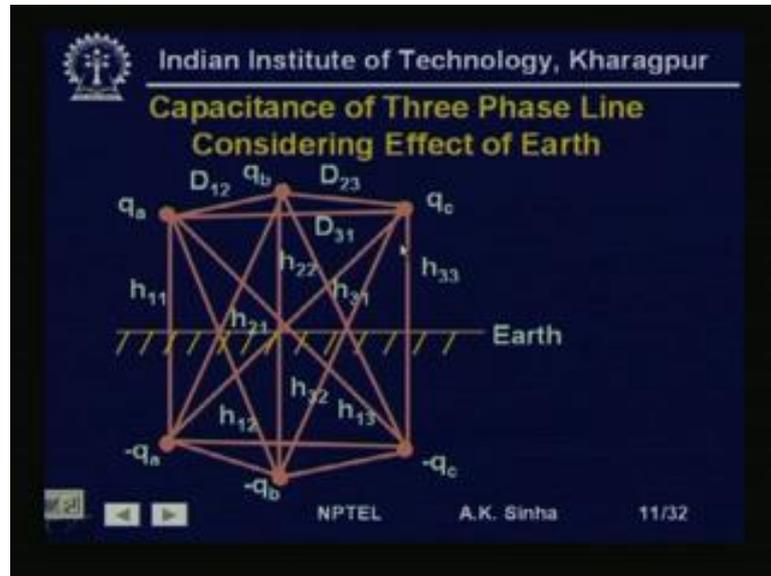
Once we have got this voltage, we can calculate the line to line capacitance as C_{xy} is equal to q by V_{xy} . So, now this is simply q divided by V_{xy} , that we have calculated this will come out to be $\pi\epsilon$ by $\log n D$ by r minus $\log n H_{xy}$ by H_{xx} farad per meter. Now, as we had seen earlier, the capacitance to neutral or capacitance to ground will be equal to twice C_{xy} , because the earth surface or the ground will have a potential which will be half that of between x and y .

So, we can write C_n is equal to $2 C_{xy}$, which is equal to twice $\pi\epsilon$ divided by $\log n D$ by r minus $\log n H_{xy}$ by H_{xx} . So, in this way we can calculate the capacitance considering the effect of ground. Now, here what we are finding that, what how this effect of ground is taken into account. If you see this expression and compare it with the expression for the single phase capacitance of a single phase transmission line, then we are saying seeing that, it is this term which is an addition or for taking the effect of earth.

And here, we can see that if the conductors are very much above the ground compared to the distance between them. Then, D_{xy} and D_{xx} will be almost equal, that is this distance and this distance will be almost equal. If the conductors are very much above the ground that is H is very large. And in that case, we find that the effect of ground will be negligible. So, if the conductors are not far off above the ground, as compared to the distance between the phase conductors.

Then, the earth does affect the capacitance and the effect as in increasing the capacitance as compared to when we have not considered the effect of earth, because this total term is now getting reduced.

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Now, we will talk about the capacitance of 3 phase line considering the effect of earth. Now, here we have 3 conductors a, b and c placed at position 1, 2 and 3. The distance between these conductors are D_{12} , which is the distance between a and b. D_{23} which is distance between b and c, and D_{31} which is distance between c and a. The conductors are carrying a charge of q_a , the phase a conductor has a charge q_a per meter. Phase b conductor has charge q_b per meter and phase c conductor has charge q_c per meter.

Now, these conductors are placed above ground. And if we have to take into account the effect of ground. Then we have to consider the image conductors. The image conductors will be for the phase a conductor. Here which will be again at a distance, which will be below the ground which will be equal to the height of this conductor above the ground. So, this will be an image conductor here with a charge, which will be negative of that of the conductor here.

Similarly, for phase b conductor, we have a image conductor here with a charge minus q_b . And for phase conductor c, we have an image conductor with a charge minus q_c . Now, the distance is from the phase conductors to the image conductors are given as

from conductor a to its image a' it will be h_{11} . That is considering this is position one. Similarly, for phase a conductor and image of b, we will have the distance h_{12} . For the distance from phase b conductor to image of a, it will be h_{21} and so on. So, we have all these distances which are shown in this figure.

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$$V_{ab} = \frac{1}{2\pi\epsilon} \left[q_a \left(\ln \frac{D_{12}}{r} - \ln \frac{h_{12}}{h_{11}} \right) + q_b \left(\ln \frac{r}{D_{12}} - \ln \frac{h_{22}}{h_{12}} \right) + q_c \left(\ln \frac{D_{23}}{D_{31}} - \ln \frac{h_{23}}{h_{31}} \right) \right]$$

Now, we can calculate the voltage between 2 phase conductors. So, we will calculate that voltage V_{ab} , the voltage between conductor a and b. And this will be given by $\frac{1}{2\pi\epsilon} q_a \left(\ln \frac{D_{12}}{r} - \ln \frac{h_{12}}{h_{11}} \right)$. It will be $\log \frac{D_{12}}{r}$ minus $\log \frac{h_{12}}{h_{11}}$, ((Refer Time: 22:02)) that is $\log \frac{D_{12}}{r}$. That is from this conductor distance of this from phase b conductor D_{12} .

And distance of this conductor from itself that is D_{11} and divided by the distance from itself that is D_{11} , which is equal to r . So, we have this first term taking into account that part. Now, because of the image conductor, that is placed here. Again we will have minus q_a is the charge on this conductor. And the distance is from this to b, it will be h_{21} and distance of from this to a will be h_{11} . Therefore, we have this minus $\log \frac{h_{12}}{h_{11}}$, because minus q_a is the charge, so minus $\log \frac{h_{12}}{h_{11}}$.

Similarly, for charge on conductor b, and its image we will get the term $\frac{1}{2\pi\epsilon} q_b \left(\ln \frac{r}{D_{12}} - \ln \frac{h_{22}}{h_{12}} \right)$. Plus due to the charge on conductor c and its image we will have the term $\frac{1}{2\pi\epsilon} q_c \left(\ln \frac{D_{23}}{D_{31}} - \ln \frac{h_{23}}{h_{31}} \right)$.

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$$C_n = \frac{2\pi\epsilon}{\ln \frac{D_{eq}}{r} - \ln \frac{\sqrt[3]{h_{12}h_{23}h_{31}}}{\sqrt[3]{h_{11}h_{22}h_{33}}}} \quad \text{F/m}$$

Three Phase Line with Earth Return

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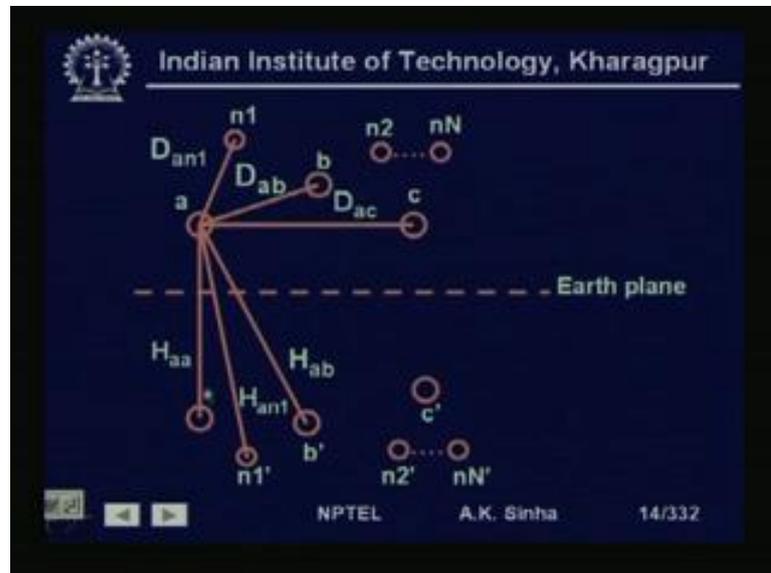
So, just as we have calculated the voltage between the conductor a and b. We can also calculate in the same way the voltage between conductors a and c. So, we will get the voltage V_{ac} in that case, if we add these two voltages V_{ab} plus V_{ac} , we had seen this is equal to $3V_{an}$. In this way we can calculate the voltage V_{an} , that is voltage between phase a conductor and the ground or the neutral, and since we know of the charge on conductor a as q_a . Therefore, we can calculate the capacitance C_n for or C_{an} for the conductor a. That is the capacitance for phase a conductor to ground will be coming out to be equal to twice pi epsilon divided by $\ln \frac{D_{eq}}{r}$ minus $\ln \frac{\sqrt[3]{h_{12}h_{23}h_{31}}}{\sqrt[3]{h_{11}h_{22}h_{33}}}$. Now, here again what we are seeing is that, the term $\ln \frac{\sqrt[3]{h_{12}h_{23}h_{31}}}{\sqrt[3]{h_{11}h_{22}h_{33}}}$ is the effect of earth on the capacitance.

Now, this is getting subtracted in the denominator. So, the effect of ground when we consider for calculating the capacitance, the capacitance will be higher than if we neglect the effect of ground. Again here we see if the conductors of the phase conductors a, b, c are vary for above the ground compared to the distance between them. Then h_{12} , h_{23} and h_{31} will be very much nearly equal to h_{11} , h_{22} and h_{33} . And therefore, this term will come out to be 0, that is the effect of ground will be negligible.

However, since these distances or between the phase conductors, and the distance between phase conductor on the ground are of the same magnitude. The effect of ground

is basically to increase the capacitance of the transmission line. Now, we will talk about 3 phase line with earth return.

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So, again we take into consideration a 3 phase system, with neutral wires of the ground wires on top of the phase conductors. This is the configuration that we have for a 3 phase EHV system. Now, if the phase conductors are fully transposed and are carrying balance current, then there will be no current flowing in the earth conductors or in the ground. However, when there is unbalanced current flowing through the phase conductors. There is going to be some current which will be flowing in the earth conductors or the ground conductors, and also in the ground itself.

As we had seen earlier we can take care of this by means of using the effect of images as we had done for calculating inductance, and calculating the resistance. So, here again since, these conductors are above the ground what we are doing is? We are considering the image conductors below the overhead conductors. Again at a distance which is equal to the distance of the conductor above the ground.

So, we are taking an image conductor and using the method of images. Now, we will have instead of 3 conductors and n neutral conductors. We will have now 6 conductors and $2n$ neutral conductors in the system, because we have 3 plus n conductors for the neutral as the image conductors also.

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$$\begin{aligned}
 V_{kk'} &= \frac{1}{2\pi\epsilon} \left[\sum_{m=a}^{nN} q_m \ln \frac{H_{km}}{D_{km}} - \sum_{m=a}^{nN} q_m \ln \frac{D_{km}}{H_{km}} \right] \\
 &= \frac{2}{2\pi\epsilon} \sum_{m=a}^{nN} q_m \ln \frac{H_{km}}{D_{km}}
 \end{aligned}$$

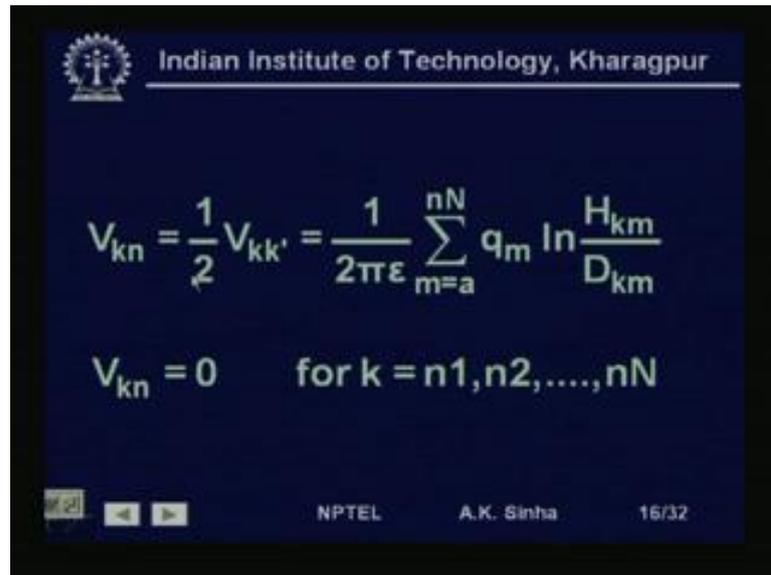
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Now, for this system, again we can find out the voltage between any conductor and its image. That will be given by $V_{kk'}$. For any conductor k , we can write the voltage between the conductor k and its image k' . That will be equal to $\frac{1}{2\pi\epsilon}$ times the summation of m is equal to a to nN , where nN is the total number of conductors in the system into q_m , the charge on conductor m $\log \frac{H_{km}}{D_{km}}$.

The distance from the image conductor k' to the m th conductor above the ground, divided by D_{km} the distance between the k th conductor and the m th conductor. Minus summation m is equal to a to nN , that is to for all the conductors in the system. Q_m the charge on m th conductor into $\log \frac{D_{km}}{H_{km}}$. That is again the distance between the image conductor k' to the conductor m divided by, distance between the conductor k and conductor m divided by the distance between the k th conductor.

And the image conductor m , that is this part is coming because of the image conductor m . This part is coming because of the overhead conductor m . So, because the image conductor carries a negative charge to that of the overhead conductor above. So, this negative sign is coming here. So, if we add this we will get this as equal to $\frac{2}{2\pi\epsilon}$ times the summation m is equal to a to nN $q_m \log \frac{H_{km}}{D_{km}}$. That is we can multiplied with by minus 1, then we can inward this. So, this will be plus sigma m is equal to a to nN $q_m \log \frac{H_{km}}{D_{km}}$ and then we can add them.

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$$V_{kn} = \frac{1}{2} V_{kk'} = \frac{1}{2\pi\epsilon} \sum_{m=a}^{nN} q_m \ln \frac{H_{km}}{D_{km}}$$
$$V_{kn} = 0 \quad \text{for } k = n1, n2, \dots, nN$$

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Now, the voltage between the k th conductor and the neutral, or the earth will be equal to half of that between the conductor k and its image k' . Therefore, V_{kn} will be equal to half $V_{kk'}$ which will be equal to $\frac{1}{2\pi\epsilon}$ because that 2 is cancelled out with this 2 here. So, it is $\frac{1}{2\pi\epsilon}$ summation m is equal to a to nN of $q_m \log \frac{H_{km}}{D_{km}}$.

Now, since the ground conductors which are on top of the phase conductors. Since, they are grounded at regular intervals by means of tower footing. Therefore, the voltage of these conductors with respect to neutral or ground is going to be 0, because these conductors are at ground potential. Therefore, V_{kn} is equal to 0 for k is equal to $n+1$, $n+2$ up to nN . That is expected for the phase conductors, all these ground conductors than ground conductors their voltage is going to be 0.

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$$\begin{bmatrix} V_{an} \\ V_{bn} \\ V_{cn} \\ 0 \\ \vdots \\ 0 \end{bmatrix} = \begin{bmatrix} P_{aa} & P_{ab} & P_{ac} & P_{an1} & \dots & P_{anN} \\ P_{ba} & P_{bb} & P_{bc} & P_{bn1} & \dots & P_{bnN} \\ P_{ca} & P_{cb} & P_{cc} & P_{cn1} & \dots & P_{cnN} \\ P_{n1a} & P_{n1b} & P_{n1c} & P_{n1n1} & \dots & P_{n1nN} \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ P_{nNa} & P_{nNb} & P_{nNc} & P_{nNn1} & \dots & P_{nNnN} \end{bmatrix} \begin{bmatrix} q_a \\ q_b \\ q_c \\ q_{n1} \\ \vdots \\ q_{nN} \end{bmatrix}$$

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Now, we can put this whole equation into a matrix form as shown here. V_{an} , V_{bn} , V_{cn} and V_{n1} , V_{n2} and up to V_{nN} , these are 0's is equal to a matrix of P's into q_a the charge on conductor a, q_b the charge on conductor b, q_c the charge on conductor c, q_{n1} up to q_{nN} the charge on neutral, conductors or the ground conductors which are placed above the phase conductors. That is we are talking about the charges on these ((Refer Time: 34:15)) conductors, n_1 n_2 up to n_N .

Now, here we see, we can divide this P matrix which will be 3 plus n_N matrix, 3 plus n_N by 3 plus n_N matrix. This matrix we can divide into 4 sub-matrices P A, P B, P C and P D, where P A is a 3 by 3 matrix of which relates the voltage with respect to charge on the phase conductors. P B is going to be are 3 by n matrix, P C is a n rows and 3 column that is n by 3 matrix. And P D is a n rows and n column, that is n by n matrix for all the ground conductors.

And see P A is relating the phase conductors, P B is relating the phase conductors with the charges on the ground conductors. P C is relating the voltage on the neutral conductors, with respect to the charges on the phase conductors. And P D is relating the voltage on the neutral conductors, with respect to the charges on the neutral conductors.

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$$P_{km} = \frac{1}{2\pi\epsilon} \ln \frac{H_{km}}{D_{km}} \text{ m/F}$$

$$\begin{bmatrix} V_p \\ 0 \end{bmatrix} = \begin{bmatrix} P_A & P_B \\ P_C & P_D \end{bmatrix} \begin{bmatrix} q_p \\ q_n \end{bmatrix}$$

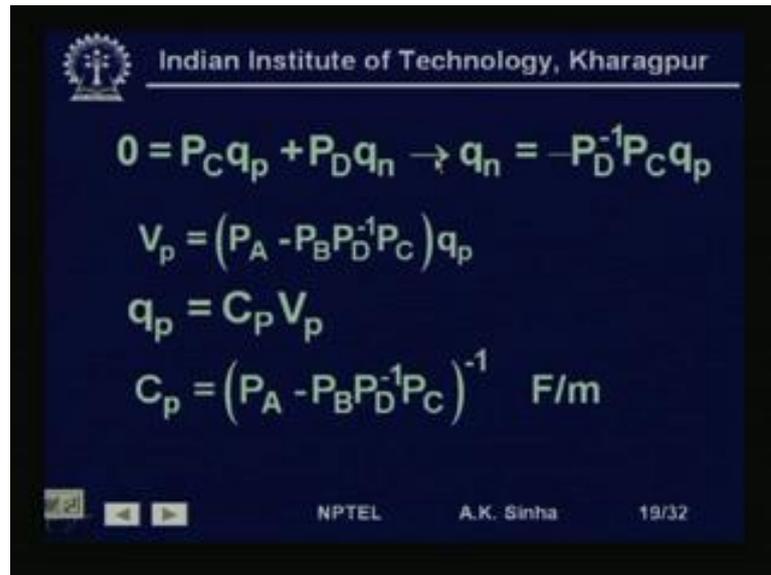
$$V_p = P_A q_p + P_B q_n$$

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Here P_{km} , that is any of these terms P_{ka} , P_{kb} , P_{kc} or P_{kn} , is given by the relationship $\frac{1}{2\pi\epsilon} \ln \frac{H_{km}}{D_{km}}$ meters per farad. Now, this matrix which we had this big matrix relationship can be written in a shorter form as V_p which is the voltage for the phase conductors. And 0 which is the voltage for all the n ground conductors is equal to P_A , P_B , P_C , P_D which we had already defined earlier.

And q_p is the charges on the phase conductors. That is q_a , q_b , q_c and q_n is the charges on the neutral conductors q_{n1} , q_{n2} , up to q_{nN} . Now, from this relationship we can write this as V_p is equal to P_A into q_p plus P_B into q_n . Similarly, we can write 0 is equal to P_C into q_p plus P_D into q_n .

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$$0 = P_C q_p + P_D q_n \rightarrow q_n = -P_D^{-1} P_C q_p$$
$$V_p = (P_A - P_B P_D^{-1} P_C) q_p$$
$$q_p = C_p V_p$$
$$C_p = (P_A - P_B P_D^{-1} P_C)^{-1} \text{ F/m}$$

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So, 0 is equal to $P_C q_p + P_D q_n$, these results send to q_n is equal to that is we can take this part on the other side. So, this becomes minus $P_C q_p$ is equal to $P_D q_n$. And again pre multiplying both sides by P_D inverse we will get q_n is equal to minus of P_D inverse into P_C into q_p . Now, if we substitute the value of q_n into this equation, then we will get V_p is equal to P_A minus P_B into P_D inverse P_C into q_p . We can write this relationship as q_p is equal to C_p into V_p .

We know the charge is product of capacitance and voltage. So, q_p will be equal to C_p into V_p and where C_p will be equal to the inverse of this term. That is inverse of P_A minus P_B , P_D inverse P_C . Now, this C_p will be a 3 by 3 matrix which relates the capacitances between the phases or the 3 phase conductors. Now, here what we have done by doing all this, is we have eliminated the effect of the ground conductors. That is the ground currents which were flowing that effect is included by modifying the phase conductor capacitances.

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$$C_p = \begin{bmatrix} C_{aa} & C_{ab} & C_{ac} \\ C_{ab} & C_{bb} & C_{bc} \\ C_{ac} & C_{bc} & C_{cc} \end{bmatrix} \quad \text{F/m}$$

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So, C_p is a 3 by 3 matrix, C_{aa} the capacitance of a with respect to a C_{ab} between the a and b. C_{ac} between a and c, similarly C_{ba} between a and b, C_{bb} the capacitance between b. And it is image C_{cc} is between C_{bc} is between b and c and so on. So, C_p is giving us the capacitance for the 3 phase conductor system. Now, if the line is fully transposed, then we will have the same capacitances for all the 3 phase conductors. As well as the same capacitance between the 2 phase conductors. So, phase to neutral conductor capacitance, as well as the capacitance between 2 phases will be same, for all the 3 conductors.

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$$\hat{C}_p = \begin{bmatrix} \hat{C}_{aa} & \hat{C}_{ab} & \hat{C}_{ab} \\ \hat{C}_{ab} & \hat{C}_{aa} & \hat{C}_{ab} \\ \hat{C}_{ab} & \hat{C}_{ab} & \hat{C}_{aa} \end{bmatrix} \quad \text{F/m}$$

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Therefore, \hat{C}_{aa} is equal to \hat{C}_{bb} and will be equal to \hat{C}_{cc} . So, the three will have the same capacitance to neutral, whereas \hat{C}_{ab} and \hat{C}_{bc} will also be same. So, we are for a transpose line system, we are representing them with hat which shows that. This line is a this capacitance is for transpose line, not to confuse with the capacitance that we had calculated earlier.

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$$\hat{C}_{aa} = \frac{1}{3}(C_{aa} + C_{bb} + C_{cc}) \quad \text{F/m}$$

$$\hat{C}_{ab} = \frac{1}{3}(C_{ab} + C_{bc} + C_{ac}) \quad \text{F/m}$$

$$\hat{Y}_p = j\omega C_p = j(2\pi f)C_p \quad \text{S/m}$$

$$\hat{Y}_p = j\omega \hat{C}_p = j(2\pi f)\hat{C}_p \quad \text{S/m}$$

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Now, the relationship which governs this capacitance is \hat{C}_{aa} is the average of C_{aa} , C_{bb} and C_{cc} . Because, each phase conductor is occupy the 3 positions for 1 3rd length of the line. Similarly, \hat{C}_{ab} which will be equal to \hat{C}_{bc} and \hat{C}_{ac} , for the transposed line this \hat{C}_{ab} will be equal to 1 3rd of C_{ab} plus C_{bc} plus C_{ac} , that is the average value of the capacitance between the phases a b, b c and c a. Once we have calculated the capacitance, we can calculate the admittance very easily by just multiplying it by $j\omega$.

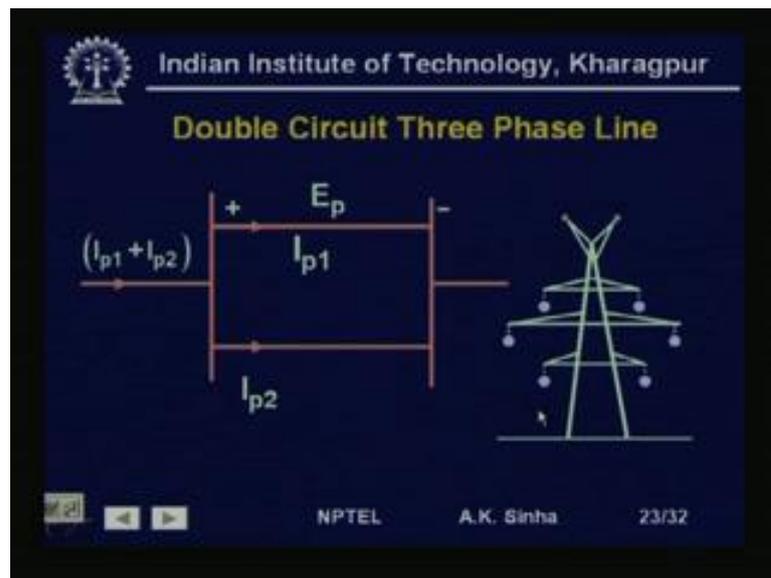
So, \hat{Y}_p or the admittance for the 3 phase system with ground wires will be given by this \hat{Y}_p which is a 3 by 3 matrix. Again this will have the terms $j\omega$ into C_p , which will be j into twice $\pi f C_p$, where C_p again as we have seen earlier is a 3 by 3 matrix. Same thing will happen for the transposed line. That is \hat{Y}_p equal to $j\omega \hat{C}_p$ plus j into twice $\pi f \hat{C}_p$ Siemens per meter.

So, in this way we have seen that, we can calculate the capacitance for any general system of 3 phase conductors. That is 3 phase conductors with any number of neutral

wires or the ground wires on top of that. Next, we will talk about double circuit line. Now, in double circuit line as we know most of the time when the power demand to an area increases, we would use instead of 1 circuit, 2 circuits. And both these circuits are running parallel to each other mostly on the same tower.

So, since these two circuits are running parallel to each other. And are on the same tower the distance between the conductors of the two circuit, is not large. Because, this distance is not large, the current flowing in them is going to effect the magnetic field of the current flowing in the other circuit. And similarly, also because the voltage of 1 circuit is going to produce electric filed, which is going to effect the electric field produced by the voltages in the other circuit. That means, there is mutual effect which takes place between these two circuits. Because, they are physically not very far off. So, they have effect from one on the other.

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Such a system we are showing here, here we have a three phase line this is one circuit and this is another circuit, which is placed here. So, this is a double circuit system, here we are showing this double circuit line. This is one circuit this is another circuit connecting two bus-bars or two sub-stations. Now, the current flowing in one circuit is I_{p1} , the current flowing in the other circuit is I_{p2} . Where I_p is basically a three element vector which consists of I_a , I_b and I_c .

So, we have I_{a1} , I_{b1} , I_{c1} of the circuit 1 and I_{a2} , I_{b2} , I_{c2} for the circuit 2. Now, this current flowing here from one circuit will be I_{p1} plus I_{p2} which gets divided into I_{p1} I_{p2} . And maybe it is getting connecting on this side this is this is shown that we are showing. We are talking about the effect of the two currents flowing in these two circuits. How they are going to effect the series impedance of the transmission line. As well as how they are going effect the shunt admittance of the transmission system. So, first we will take up the series impedance.

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Series Impedance

$$\begin{bmatrix} E_p \\ E_p \end{bmatrix} = Z_p \begin{bmatrix} I_{p1} \\ I_{p2} \end{bmatrix}$$

$$\begin{bmatrix} I_{p1} \\ I_{p2} \end{bmatrix} = Z_p^{-1} \begin{bmatrix} E_p \\ E_p \end{bmatrix} = \begin{bmatrix} Y_A & Y_B \\ Y_C & Y_D \end{bmatrix} \begin{bmatrix} E_p \\ E_p \end{bmatrix} = \begin{bmatrix} (Y_A + Y_B) \\ (Y_C + Y_D) \end{bmatrix} E_p$$

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Now, for the two circuits we can write, the relationship E_{p1} is equal to Z_{p1} into I_{p1} and E_{p2} is equal to Z_{p2} into I_{p2} . But, since these two circuits are close together there is mutual coupling. So, it will not be right to write separate equations for the two. In fact, what we have here is we are considering a system of 6 conductors, instead of 3 conductors.

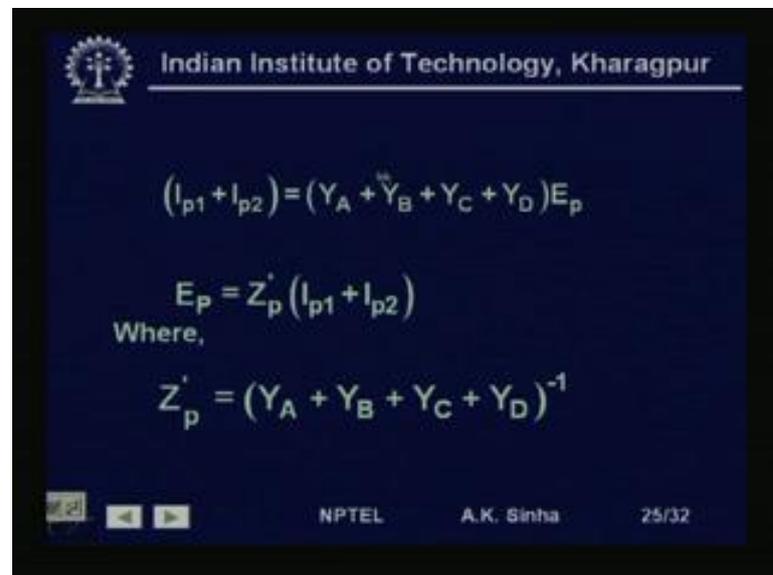
Again since we see that, ((Refer Time: 47:25)) these two circuits are connected under two ends. So, the voltage drop between them is going to be same. So, the voltage drop E_{p1} is same as E_{p2} which is equal to E_p . So, we can write E_p for circuit 1 and E_p for circuit 2 is equal Z_p into I_p for circuit 1 into I_p for circuit 2. And Z_p is going to be a 6 by 6 matrix of the series impedance.

Now, from this relationship, we can write I_{p1} , I_{p2} is equal to Z_p inverse into E_p E_p . Because, E_{p1} , E_{p2} are same, so we are writing E_p for that. So, we are from here we

are calculating this I_{p1} and I_{p2} . So, we are pre multiplying both sides by Z_p inverse. So, we get I_{p1} , I_{p2} is equal to now Z_p inverse E_p . Now, Z_p inverse will be admittance and this will be again a 6 by 6 matrix which we can divide into 4 sub matrices Y_A , Y_B , Y_C , Y_D . Where each of these sub matrices are going to be a 3 by 3 matrix.

So, this is equal to $Y_A Y_B Y_C Y_D E_p$. And this is equal to Y_A into E_p plus Y_B into E_p , so Y_A plus Y_B into E_p and Y_C into E_p plus Y_D into E_p , so Y_C plus Y_D into E_p . So, now we can write if we add the two currents I_{p1} and I_{p2} .

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$$(I_{p1} + I_{p2}) = (Y_A + Y_B + Y_C + Y_D)E_p$$

$$E_p = Z_p' (I_{p1} + I_{p2})$$

Where,

$$Z_p' = (Y_A + Y_B + Y_C + Y_D)^{-1}$$

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Then, we get I_{p1} plus I_{p2} is equal to Y_A plus Y_B plus Y_C plus Y_D into E_p . That is if you see from here, if we have I_{p1} is equal to Y_A plus Y_B into E_p and I_{p2} is equal to Y_C plus Y_D into E_p . So, if we add them we are going to get this I_{p1} plus I_{p2} is equal to Y_A plus Y_B plus Y_C plus Y_D into E_p . And this equation we can again solve for E_p . Then, E_p will be equal to Z_p dash into I_{p1} plus I_{p2} , where Z_p dash is nothing but the inverse of this matrix. Now, here if you look at this matrix, this is sum of this 3 by 3 matrix plus this 3 by 3 matrix, solve these matrixes are 3 by 3. So, Z_p dash is going to be a 3 by 3 matrix.

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Shunt Admittance

$$\begin{bmatrix} q_{p1} \\ q_{p2} \end{bmatrix} = C_p \begin{bmatrix} V_p \\ V_p \end{bmatrix} = \begin{bmatrix} C_A & C_B \\ C_C & C_D \end{bmatrix} \begin{bmatrix} V_p \\ V_p \end{bmatrix} = \begin{bmatrix} (C_A + C_B) \\ (C_C + C_D) \end{bmatrix} V_p$$

$$(q_{p1} + q_{p2}) = C_{Peq} V_p$$

$$C_{Peq} = (C_A + C_B + C_C + C_D)$$

$$Y_p' = j\omega C_{Peq}$$

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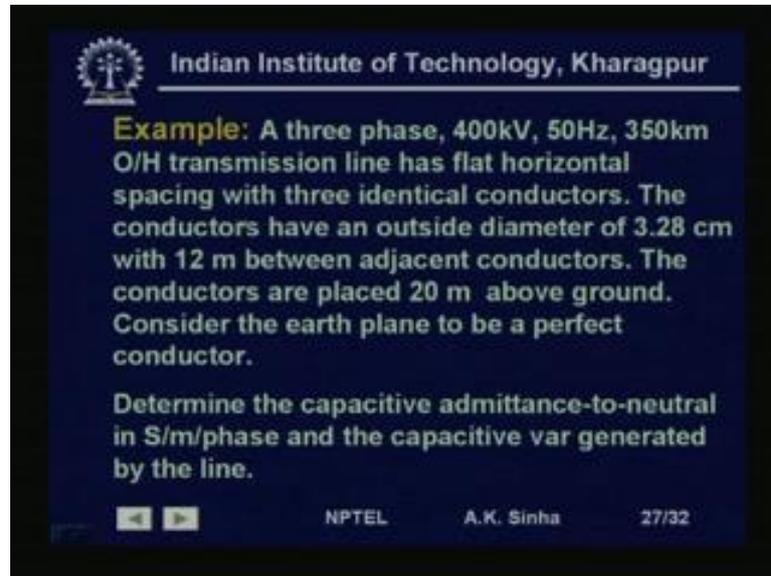
Now, we will talk about the Shunt Admittance for this double circuit line. Again in the same way as we have done for a single circuit line. We can write down the relationship for q_p for circuit 1 and q_p for circuit 2. Where, q_p will be the charges on phase conductors a, b and c. So, q_{p1} is $q_{a1} \ q_{b1} \ q_{c1}$, q_{p2} is $q_{a2} \ q_{b2}$ and q_{c2} . So, this is a vector having 6 rows C_p will be a 6 by 6 matrix.

And V_p again is the voltage of the phase conductors a, b and c for circuit 1 and circuit 2. Since, these two circuits are in parallel. Therefore, the voltages are going to be same, therefore instead of V_{p1} and V_{p2} we are writing same as V_p and V_p . Now, this C_p which is a 6 by 6 matrix can be divided into 4 sub-matrices C_A, C_B, C_C, C_D . So, we have got C_A into V_p plus C_B into V_p , so C_A plus C_B into V_p . C_C into V_p plus C_D into V_p , that is C_C plus C_D into V_p is equal to $q_{p1} \ q_{p2}$.

From here again we get q_{p1} is equal to C_A plus $C_B \ V_p$, q_{p2} is equal to C_C plus C_D into V_p . Therefore, if we add these two we get q_{p1} plus q_{p2} is equal to C_p equivalent into V_p . Now, is this C_p is going to be C_p equivalent is going to be a 3 by 3 matrix instead of a 6 by 6 matrix C_p . So, where C_p equivalent is nothing but equal to C_A plus C_B plus C_C plus C_D , and this is a 3 by 3 matrix and therefore, we can get the shunt admittance for this double circuit line. In terms of 3 phase system, for at which will gives us a 3 by 3 matrix for the phase a, phase b and phase c, which includes the mutual effect between the two circuits. So, we will get Y_p' is equal to $j\omega C_{Peq}$. So, now

that we have seen how to calculate the capacitance taken into account, the effect of earth. And we have also seen how we can calculate the series, or shunt admittance for a double circuit line, taking into the account of mutual effects.

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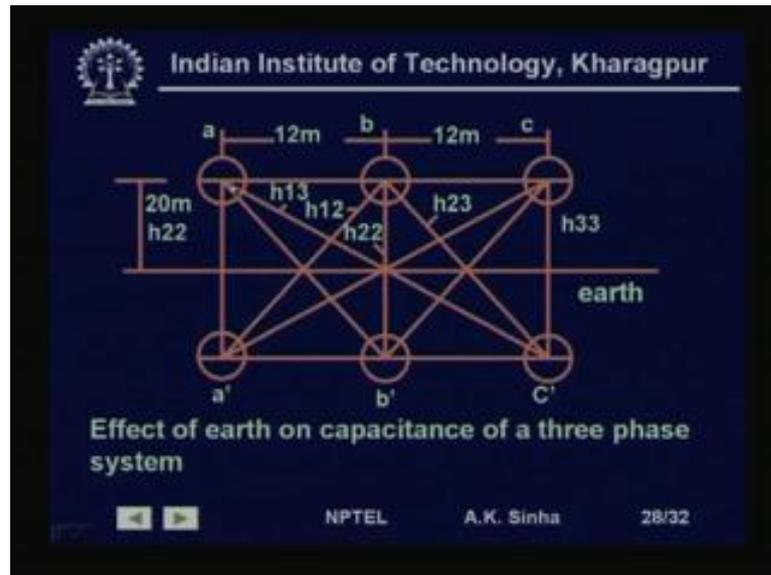
Example: A three phase, 400kV, 50Hz, 350km O/H transmission line has flat horizontal spacing with three identical conductors. The conductors have an outside diameter of 3.28 cm with 12 m between adjacent conductors. The conductors are placed 20 m above ground. Consider the earth plane to be a perfect conductor.

Determine the capacitive admittance-to-neutral in S/m/phase and the capacitive var generated by the line.

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Well, let us take an example to illustrate some of the concepts that we learn today. We consider a 3 phase 400 kV, 50 Hertz, 350 kilometer overhead transmission line with flat horizontal spacing with three identical conductors. The conductors have an outside diameter of 3.28 centimeters with 12 meter between the adjacent conductors. The conductors are placed 20 meter above the ground, we consider the earth plane to be perfect conductor. Determine the capacitive admittance to neutral in Siemens per meter per phase and the capacitive var generated by the line. So, this is the problem that we have.

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And we can show this configuration graphically as shown here. We have the 3 conductors, a, b and c placed here, we will say that these are positions 1, 2 and 3. There are 12 meters apart from each of the conductors. Since, we are considering the ground to be a perfect conductor, we take the effect of image conductors. So, we have a image conductor of a, as a dash which is again 20 meters below the earth. Similar for b and c and we have the distances h_{ij} which is showing the distance between the conductor I with the image conductor j. So, h_{13} is the distance between conductor a and the image of conductor c and so on.

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Solution: Let h_{11} , h_{22} , h_{33} be the distances between the conductors and their mirror images. And also, h_{12} , h_{23} , h_{31} be the distances as shown in the figure on the previous slide.

We have for such systems, following the same procedure,

$$C_n = 2\pi\epsilon_0 / \left\{ \ln(D_{eq}/r) - \ln\left(\frac{h_{12}h_{23}h_{31}}{(h_{11}h_{22}h_{33})^{1/3}}\right) \right\}$$

So, we have seen that h_{11} , h_{22} , h_{33} is the distance between the conductors and their mirror images. That is h_{11} , this should be h_{11} , from this conductor to this a to a dash is the distance between image conductor this will be a 40 meters. Similarly, b to b dash will be forty meter and c to c dash will be 40 meters. So, and h_{ij} as we have said is the distance shown in the figure.

Now, we have for such a system, following the same procedure as we have shown earlier. That is if we go back ((Refer Time: 56:40)) here we have the capacitance to neutral for 3 phase system with image conductors. This is given by this relationship, we write the same relationship here. So, we have C_n is equal to twice π epsilon divided $\log_n D_{eq}$ by r minus $\log_n h_{11} h_{23} h_{31}$ divided $h_{11} h_{22} h_{33}$ a cube root of that.

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We have,
 $D_{eq} = 15.119\text{m}$
 $r = 1.64\text{ cm}$

From the diagram,
 $h_{11} = h_{22} = h_{33} = 40\text{m}$
 $h_{12} = h_{23} = (40^2 + 12^2)^{1/2} = 41.761\text{ m}$
 $h_{31} = (40^2 + 24^2)^{1/2} = 46.648\text{ m}$

Putting these values in the equation
 (1) we get $C_n = 8.2595 \times 10^{-6} \mu\text{F/m}$.

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So, now what we do is we substitute all the values, we can calculate D_{eq} as 15.119 meter which is basically the cube root of the distance between the conductors themselves. R is the radius of the conductor which is equal to 1.64, it is 3.28 divided by 2. From the diagram, we have the values by h_{11} h_{22} h_{33} as 40 meters, h_{12} h_{23} are shown here is equal to 41.761 meters, h_{31} is equal to 46.648 meters. Now, putting these values in the equations we get C_n is equal to 8.2595 into 10 to power minus 6 microfarad per meter.

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Hence, $Y_n = 2\pi \times 50 \times 8.2595 \times 10^{-12} \text{ S/m/phase}$
 $= 2.595 \times 10^{-9} \text{ S/m/phase}$

Length of the line = 350 km.

Therefore, Total $Y_n = 908 \mu\text{S}$ per phase.

Now var generated by line $Q_c = Y_n \times V_{LL}^2$

Or $Q_c = 908 \times 10^{-6} \times 400 \times 10^3 \times 400 \times 10^3$
 $= 145.358 \text{ Mvar}$

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Hence, we can calculate the admittance Y_n is equal to twice πf which is 50 into the C_n . This is C_n that is 8.2595 into 10 to power minus 12 Siemens per meter per phase, this is equal to 2.595 into 10 to power minus 9 Siemens per phase. Now, length of the line is given as three 50 kilometers, therefore total admittance will be simply multiply this by 350, this conserved to be 908 micro Siemens per phase.

Now, the var generated by the line Q_c will be equal to Y_n into V_{LL}^2 square or Q_c is equal to 908 into 10 to the power minus 6 into 400 into 10 to power minus 3 square, that is 400 into 10 to power minus 10 to power 3 into 400 into 10 to power 3, there is a 400 kilo volts. So, this conserved to be 145.358 Mvar. So, that is all discuss about the capacitance calculation. In the next class on lessons 7, we will discuss about modeling of transmission lines.

Once that we have we need we have learnt about how to calculate the parameters of the transmission line. That is the resistance, the inductance and the capacitance for the transmission line. Now, we would like to model the transmission line for analysis. So, that we will do in lesson 7.

Thank you.